# AE31002 Structural Dynamics Natural Frequency of SDOF System

Anup Ghosh

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#### Simple Harmonic Motion

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In the Static equilibrium case,  $k\Delta = w = mg$ At any intermediate position with a displacement of x, following D'Alemberts's Static Equilibrium  $m\ddot{x} = \sum F = w - k(\Delta + x)$  $m\ddot{x} + kx = 0$ 



In the Static equilibrium case,  $k\Delta = w = mg$ At any intermediate position with a displacement of x, following D'Alemberts's principle Equilibrium  $\ddot{m}\ddot{x} = \sum F = w - k(\Delta + x)$  $m\ddot{x} + kx = 0$ A 2nd order differential equation.

Let us assume a trial solution,  $x = A \cos \omega t$  or  $x = B \sin \omega t$ 

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Let us assume a trial solution,  $x = A \cos \omega t$  or  $x = B \sin \omega t$ Substituting the first one  $(-m\omega^2 + k)A \cos \omega t = 0$  $\Rightarrow \omega^2 = \frac{k}{m} \Rightarrow \omega_n = \sqrt{\frac{k}{m}}$ 

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Velocity at any instant of time

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To find out the values of the constants we need to solve a initial value problem,

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To find out the values of the constants we need to solve a initial value problem,

For 
$$t = 0$$
,  $x = x_0$ , and  $\dot{x} = v_0$   
 $x_0 = A$  and  $v_0 = B\omega_n$   
 $\Rightarrow x = x_0 \cos \omega_n t + \frac{v_0}{\omega_n} \sin \omega_n t$ 

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 $\Rightarrow x = x_0 \cos \omega_n t + \frac{v_0}{\omega_n} \sin \omega_n t$   
Also may be written as  $x = C \sin(\omega_n t + \alpha)$   
where,  $tan \alpha = \frac{x_0}{v_0/\omega_n}$ 

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## SDOF without damping

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Let,  
$$x = Ae^{\lambda t}$$

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Let,  

$$x = Ae^{\lambda t}$$
  
 $\lambda^2 + \omega_n^2 = 0 \implies \lambda = \pm i\omega_n$ 

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Let,  

$$x = Ae^{\lambda t}$$
  
 $\lambda^2 + \omega_n^2 = 0 \Rightarrow \lambda = \pm i\omega_n$   
 $x = A_1e^{i\omega_n t} + A_2e^{-i\omega_n t}$   
where  $A_1$  and  $A_2$  are constants.

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Let,  

$$x = Ae^{\lambda t}$$
  
 $\lambda^2 + \omega_n^2 = 0 \Rightarrow \lambda = \pm i\omega_n$   
 $x = A_1 e^{i\omega_n t} + A_2 e^{-i\omega_n t}$   
where  $A_1$  and  $A_2$  are constants.  
Consider the series,  
 $e^{i\omega t} = \cos \omega t + i \sin \omega t$   
 $e^{-i\omega t} = \cos \omega t - i \sin \omega t$ 

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Let.  $x = A e^{\lambda t}$  $\lambda^2 + \omega_n^2 = 0 \Rightarrow \lambda = \pm i\omega_n$  $x = A_1 e^{i\omega_n t} + A_2 e^{-i\omega_n t}$ where  $A_1$  and  $A_2$  are constants. Consider the series.  $e^{i\omega t} = \cos \omega t + i \sin \omega t$  $e^{-i\omega t} = \cos \omega t - i \sin \omega t$ Substituting the above values,  $x = (A_1 + A_2) \cos \omega_n t + i(A_1 - A_2) \sin \omega_n t$ if we consider,  $(A_1 + A_2) = \cos \phi$ ,  $i(A_1 - A_2) = \sin \phi$  $x = A \cos(\omega_n t - \phi)$ 

To find out the values of the constants we need to solve a initial value problem,

For 
$$t = 0$$
,  $x = x_0$ , and  $\dot{x} = v_0$   
 $x_0 = A \cos \phi$  and  $v_0 = A\omega_n \sin \phi$   
 $A = \sqrt{x_0^2 + (\frac{v_0}{\omega_n})^2}$  and  $tan \phi = \frac{v_0/\omega_n}{x_0}$   
 $\Rightarrow x = x_0 \cos \omega_n t + \frac{v_0}{\omega_n} \sin \omega_n t$ 

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Determine the natural frequency of the system shown in the figure. The system consists of a weight of 50.7kg to a horizontal cantilever beam through a coil spring  $k_2$ . The cantilever beam has a thickness  $t = \frac{1}{4}$  cm, a width b = 1 cm and modulus of elasticity  $E = 30 \times 10^6 \ kg/cm^2$ , and a length  $L = 12.5 \ cm$ . The coil spring has a stiffness,  $k_2 = 10.69 \ kg/cm$ .

For a cantilever beam the tip deflection  $\Delta$  due to the application of a transverse concentrated load P

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For a cantilever beam the tip deflection  $\Delta$  due to the application of a transverse concentrated load P is  $\Delta = \frac{PL^3}{3Fl}$ .

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For a cantilever beam the tip deflection  $\Delta$  due to the application of a transverse concentrated load P is  $\Delta = \frac{PL^3}{3El}$ . Corresponding spring constant or stiffnrss is  $k_1 = \frac{P}{\Delta} = \frac{3El}{L^3}$ ,

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### SDOF – Examples

For a cantilever beam the tip deflection  $\Delta$  due to the application of a transverse concentrated load P is  $\Delta = \frac{PL^3}{3EI}$ . Corresponding spring constant or stiffnrss is  $k_1 = \frac{P}{\Delta} = \frac{3EI}{L^3}$ , where  $I = \frac{bt^3}{12}$ 

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For a cantilever beam the tip deflection  $\Delta$  due to the application of a transverse concentrated load P is  $\Delta = \frac{PL^3}{3EI}$ . Corresponding spring constant or stiffnrss is  $k_1 = \frac{P}{\Delta} = \frac{3EI}{L^3}$ , where  $I = \frac{bt^3}{12}$ The system shows that it acts as two springs are in series.

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For a cantilever beam the tip deflection  $\Delta$  due to the application of a transverse concentrated load P is  $\Delta = \frac{PL^3}{3El}$ . Corresponding spring constant or stiffnrss is  $k_1 = \frac{P}{\Delta} = \frac{3El}{L^3}$ , where  $l = \frac{bt^3}{12}$ The system shows that it acts as two springs are in series. Equivalent stiffness of the system

$$k_{eq} = \{\frac{1}{k_1} + \frac{1}{k_2}\}^{-1}$$

$$k_{eq} = \{\frac{1}{60} + \frac{1}{10.69}\}^{-1} = 9.07 kg/cm^2$$

Natural frequency of the system is  $\omega = \sqrt{k_e/m} = \sqrt{9.07 \times 0.981/50.7}$ 

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Determine the natural frequency of a weight w suspended from a spring at the mid point of a simply supported beam shown below. The length of the beam is L, and its flexural rigidity is El. The spring stiffness is k. Assume the beam to be mass-less.





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The Static equilibrium position may be considered as the origin. So the equation of motion becomes m



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