AE31002 Aerospace Structural Dynamics Damped SDOF System

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Viscous Damping – the

type of damping force that could be developed in a body restrained in its motion by a surrounding viscous fluid.



The summation of forces following D'Alembert's principle $m\ddot{x} + c\dot{x} + kx = 0$

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 $m\ddot{x} + c\dot{x} + kx = 0$

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The trial solutions $x = A \sin \omega t$ or $x = B \cos \omega t$ does not satisfy the above equation where as $x = Ae^{\lambda t}$ satisfies.

$$\Rightarrow m\lambda^{2} + c\lambda + k = 0 \Rightarrow \lambda^{2} + \frac{c}{m}\lambda + \frac{k}{m} = 0 \lambda = -\left(\frac{c}{2m}\right) \pm \left[\left(\frac{c}{2m}\right)^{2} - \left(\frac{k}{m}\right)\right]^{\frac{1}{2}} x = e^{-\left(\frac{c}{2m}\right)t} \left[Ae^{\sqrt{\left(\frac{c}{2m}\right)^{2} - \left(\frac{k}{m}\right)t}} + Be^{-\sqrt{\left(\frac{c}{2m}\right)^{2} - \left(\frac{k}{m}\right)t}}\right]$$

There may be three possible cases where the portion under the radical may be positive or negative or zero for the cases over-damped or under-damped or critically-damped cases, respectively.

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Case I $\left(\frac{c}{2m}\right)^2 > \left(\frac{k}{m}\right) -$ **Over Damped Case** The solution becomes $x = A_1 e^{-\lambda_1 t} + A_2 e^{-\lambda_2 t}$ where λ_1 and λ_2 are two real roots of the equation. The system displacement will decay without any oscillation. This equation shows that there is a usual creeping back of the mass to the equilibrium position. This is a case of over-damped situation and no oscillation is possible.

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Case II $\left(\frac{c}{2m}\right)^2 < \left(\frac{k}{m}\right)$ – **Under Damped Case** Roots of the equation are imaginary. Oscillation continues for a considerable time period depending upon the damping present in the system.

$$\lambda = -\left(\frac{c}{2m}\right) \pm i \left[\left(\frac{k}{m}\right) - \left(\frac{c}{2m}\right)^2\right]^{\frac{1}{2}}$$
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Now using exponential series, $e^{i\theta} = \cos\theta + i \sin\theta$ $e^{-i\theta} = \cos\theta - i \sin\theta$

Substituting the expressions similar to the above we get, considering, $\omega_d = \left[\left(\frac{k}{m}\right) - \left(\frac{c}{2m}\right)^2 \right]^{\frac{1}{2}}$ $x = e^{-\frac{c}{2m}t} \left[A_1' e^{i\omega_d t} + A_2' e^{-i\omega_d t} \right]$ $= e^{-\frac{c}{2m}t} \left[A_1' (\cos \omega_d t + i \sin \omega_d t) + A_2' (\cos \omega_d t - \sin \omega_d t) \right]$ $= e^{-\frac{c}{2m}t} \left[(A_1' + A_2') \cos \omega_d t + i (A_1' - A_2') \sin \omega_d t \right]$

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Let, $A'_1 + A'_2 = A \sin \phi$

$$i(A_1' + A_2') = A\cos\phi$$

$$x = e^{\left(-\frac{c}{2m}t\right)} \left[A \sin(\omega_d t + \phi)\right]$$

where,

$$A^{2} = (A'_{1} + A'_{2})^{2} - (A'_{1} - A'_{2})^{2}$$

$$= A'_{1}^{2} + A'_{2}^{2} + 2A'_{1}A'_{2} - A'_{1}^{2} - A'_{2}^{2} + 2A'_{1}A'_{2}$$

$$= 4A'_{1}A'_{2}$$

$$A = 2(A'_{1}A'_{2})^{\frac{1}{2}}$$

$$\tan \phi = \frac{A'_{1} + A'_{2}}{i(A'_{1} - A'_{2})}$$

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So, roots of the equation are,

$$\lambda_1 = -\frac{c}{2m} + i\omega_d$$
$$\lambda_2 = -\frac{c}{2m} - i\omega_d$$

With a frequency, $\omega_1 = \omega_d = \left[\left(\frac{k}{m}\right) - \left(\frac{c}{2m}\right)^2 \right]^{\frac{1}{2}}$ The frequency is not same as of the case of undamped case. It is some amount less than the previous value, i.e., $\sqrt{\frac{k}{m}}$. The change is dependent on the damping parameter c and the mass of the system.

Therefore the equation of damped single degree of freedom system is

$$x = e^{\left(-\frac{c}{2m}t\right)} \left[A \sin(\omega_d t + \phi)\right]$$

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Case III $\left(\frac{c}{2m}\right)^2 = \left(\frac{k}{m}\right) -$ Critically Damped Case If c_c is the coefficient for critical damping. $c_c^2 = 4km \Rightarrow c_c = 2\sqrt{km}$ $\omega_n = \sqrt{\frac{k}{m}} \Rightarrow c_c = 2m\omega_n \Rightarrow c_c = \frac{2k}{\omega_n}$ Damping ratio $\xi = \frac{c}{c_c} = \frac{Actual Damping Coefficient}{Critical Damping Coefficient}$ $\frac{c}{2m} = \frac{\xi c_c}{2m}$ substituting the above relation

$$\frac{c}{2m} = \xi \omega_n$$

The equation for free damped single degree freedom system modifies to

$$x = e^{(-\xi\omega_n t)} \left[A \sin(\omega_d t + \phi)\right]$$

where $\omega_d = \omega_n \sqrt{1 - \xi^2}$

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$$\begin{split} \mathcal{T}_1 &= \frac{2\pi}{\omega_d} = \frac{2\pi}{\omega_n\sqrt{1-\xi^2}},\\ \lambda_{1,2} &= -\xi\omega_n \pm \sqrt{\left(\xi\omega_n\right)^2 - \omega_n^2} = \left(-\xi \pm \sqrt{\xi^2 - 1}\right)\omega_n\\ \text{This is the case of } \xi < 1 \quad \text{, i.e., All damped free vibrations.}\\ \text{when } \xi = 1 \quad \text{It is a case of critically damped one.}\\ \xi > 1 \quad \text{It is a case of over-damped one.} \end{split}$$

In case of under-damped or damped case the constants may be found out solving a initial value problem. Let, at t = 0, $x = x_0$, and $\dot{x} = v_0$ and if we substitute it to $x = e^{(-\xi\omega_n t)} [A \sin(\omega_d t + \phi)]$

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We get

$$\begin{aligned} x &= e^{(-\xi\omega_n t)} \left[x_0 \, \cos \, \omega_d t + \frac{v_0 + x_0 \xi\omega_n}{\omega_d} \, \sin \, \omega_d t \right] \\ \Rightarrow x(t) &= C e^{(-\xi\omega_n t)} \, \cos(\omega_d t - \alpha) \end{aligned}$$

where $C &= \sqrt{x_0^2 + \left(\frac{v_0 + x_0 \xi\omega_n}{\omega_d}\right)^2}$
and $\tan \alpha = \frac{v_0 + x_0 \xi\omega_n}{\omega_d x_0}$
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In case of Over-Damped System, we get from the general solution

$$x = Ae^{(-\xi + \sqrt{\xi^2 - 1})\omega_n t} + Be^{(-\xi - \sqrt{\xi^2 - 1})\omega_n t}$$

where $A = \frac{\dot{x_0} + (\xi + \sqrt{\xi^2 - 1})\omega_n x_0}{2\omega_n \sqrt{\xi^2 - 1}}$ and $B = \frac{-\dot{x_0} - (\xi - \sqrt{\xi^2 - 1})\omega_n x_0}{2\omega_n \sqrt{\xi^2 - 1}}$

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In case of Critically-Damped System, we get from the general solution

$$x = (A + Bt)e^{\omega_n t}$$

With implementation of initial conditions

$$x(t) = [x_0 + \{\dot{x}_0 + \omega_n x_0\}t] e^{\omega_n t}$$

ANIMATION of CRITICALLY DAMPED SYSTEM

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